



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

.

i Leinen in der Gertreite

are the second

Accession For NTIS GRA&I DIEC TAB Distribution/ Availability Codes Avail and/or Special

Technical Report -

GLASSES FOR FIBER-OPTIC SENSORS

D. H. Blackburn, A. Feldman, and R. M. Waxler

October 1982

Prepared for the Naval Research Laboratory

Monitor: N. Lagakos Principal Investigator: A. Feldman

Period Covered: October 1, 1981-September 30, 1982

N00173-82-F-D644

This document has been approved for public release and sale; its distribution is unlimited.

06 15

GLASSES FOR FIBER-OPTIC SENSORS

1. Objective

To measure the relevant optical and mechanical properties of commercial glasses and glasses prepared at the National Bureau of Standards for the purpose of determining their suitability as fiber-optic sensor materials.

2. Introduction

The Department of the Navy is interested in the development of fiberoptic sensors for the detection of underwater acoustic waves. An advantage
of such sensors over conventional piezoelectric sensors is their insensitivity
to electromagnetic interference. However, a source of noise in such sensor
systems is expected to arise from optic path variations due to temperature
and pressure fluctuations in the fiber-optic leads connected to the sensors.
In order to minimize this noise, a program has been instituted at the Naval
Research Laboratory to develop fibers that are insensitive to pressure and
temperature fluctuations. In order to assist with this program, the Glass
Group of the National Bureau of Standards has been preparing experimental
glasses and measuring their relevant mechanical and optical properties.

The work this year has centered on the development of cladding glasses for pressure insensitive fibers. The accomplishments have been: (a) the synthesis of eight glasses of varying composition for the minimization of linear thermal expansion coefficient; (b) the measurement of elastic moduli and thermal expansion coefficients of the aforementioned glasses; (c) the development of glasses with linear thermal expansion coefficients comparable to Pyrex; (d) the fabrication of a cladding preform from one of the NBS produced glasses which was selected for optimum values of bulk modulus and linear thermal expansion coefficient so as to produce a pressure insensitive fiber; (e) the provision of bulk specimens and thin rods to EOTEK Corporation

ج بي ا

per instructions from the contract monitor; and (f) the filing of an invention disclosure with the NBS patent attorney to ascertain whether the glass compositions formulated at NBS merit a patent. $76 p_{\rm c}/$

3. Results

It has been pointed out that substrate materials for pressure insensitive fiber-optic leads should have a large bulk modulus and a small thermal expansion coefficient. To this end, NBS has been preparing a series of experimental glasses. In the previous year, in a series of eleven glasses, we had shown that the gradual addition of Ta_2O_5 and removal of CaO from a calcium aluminate based glass formulation led to glasses with both a large bulk modulus and a decreasing linear thermal expansion coefficient. For the present year, eight additional experimental glasses were synthesized with the hope of further decreasing the thermal expansion coefficient without adversely affecting the bulk modulus.

The method of specimen preparation and the measurement of elastic moduli and thermal expansion were presented in our previous report and so will not be discussed here. Table 1 summarizes the results of this year's study and the study of the previous year. The eight glasses studied this year are denoted by K-1780 and higher. It was found that as the concentration of Ta₂O₅ was increased, the linear thermal expansion coefficient reached a minimum value and then began to increase. Two glasses, K-1824 and K-1825, had Nb₂O₅ substituted for Ta₂O₅; no significant change was found in the bulk modulus, but the linear thermal expansion appeared to increase slightly.

Some B₂O₃ was added to glasses K-1847 and K-1848 as small amounts of this substance are known to decrease expansion coefficients. Indeed, K-1848 had the smallest expansion coefficient in the series. However, the bulk modulus showed a significant decrease.

Based on the results for the nineteen glasses, it was decided that glass K-1780 had the best combination of properties for the production of a cladding preform. This glass has a respectfully large bulk modulus and a linear thermal expansion coefficient comparable to Pyrex. A cladding preform of this glass was fabricated at NBS and shipped to EOTEK Corporation which is under contract with NRL for prototype drawing of fibers. EOTEK also required bulk material and some thin rods so as to study the fiber drawing properties of the NBS glass prior to the use of the preform; these specimens were prepared and have been sent to EOTEK.

The glasses we have formulated have some unique properties which make them useful for a variety of applications. We have, therefore, prepared an invention disclosure for the NBS patent attorney to evaluate. A copy of this disclosure is attached; it outlines some of the more important applications for these glasses.

References

N. Lagakos and J. A. Bucaro, "Pressure Desensitization of Optical Fibers,"
 Appl: Opt., 20, 2716 (1981).

Table 1.

Properties of NBS Prepared Glasses

(10 ¹¹ 04/m/cm ²) 25 25 10 10 10 20 25 20 10 10 10 25 27 20 20 10 10 10 25 28 20 10 10 10 25 29 25 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 20 20 10 10 10 25 21 20 20 10 10 10 25 22 20 10 10 10 25 23 20 10 10 10 25 24 20 8.89 0.284 25 20 10 10 25 20 0.284 26 20 20 10 10 25 25 27 20 20 20 20 25 25 28 20 20 20 20 25 29 20 20 20 20 25 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 20 2	5 2	Glass No.	CaO	A1203	M	T102	TiO ₂ ZrO ₂	SfO2	Ta ₂ 0s	Nb ₂ 0 ₅	. B ₂ O ₃	Young's Modulus	Shear	Shear Bulk Modulus Modulus	Pofsson's Ratio	a(10 ⁻⁶ /K)
25 26 10 10 20 11.62 4.52 9.01 0.286 25 20 10 10 25 11.45 4.45 8.92 0.286 30 15 10 10 25 10 11.45 4.45 8.92 0.286 20 10 10 10 25 10 11.45 4.45 8.92 0.286 20 10 10 10 25 15 15 15 11.45 4.45 8.89 0.286 20 10 10 10 25 10 11.45 4.45 8.89 0.286 20 10 10 10 25 10 11.45 4.45 8.89 0.281 10 20 10 25 10 11.45 4.45 8.89 0.281 20 10 10 25 20 11.50 4.65 4.65 4.65 4.65												3	10 ¹¹ dyn/c	,m ²)		at 20 °C
25 20 10 10 25 11.45 4.45 8.92 0.286 30 15 10 10 25 10 11.31 4.40 8.92 0.286 25 10 10 10 25 10 11.20 4.45 8.92 0.286 20 20 10 10 25 10 11.46 4.46 8.80 0.286 20 20 10 10 25 10 11.46 4.46 8.80 0.281 20 20 10 10 25 20 11.46 4.46 8.80 0.281 20 20 10 10 25 20 11.46 4.46 8.80 0.281 10 10 10 25 20 20 4.45 8.86 0.281 10 10 10 25 20 20 4.65 4.63 7.71 0.281 20 <th>7</th> <th>1291</th> <th>25</th> <th>52</th> <th>97</th> <th>27</th> <th>25</th> <th>70</th> <th></th> <th></th> <th></th> <th>11.62</th> <th>4.52</th> <th>9.01</th> <th>0.285</th> <th>6.49</th>	7	1291	25	52	97	27	25	70				11.62	4.52	9.01	0.285	6.49
30 15 10 10 25 10 11.31 4.40 8.81 0.286 25 10 10 10 10 25 15 11.20 4.37 8.52 0.281 20 20 10 10 25 15 11.46 4.46 8.88 0.285 20 20 10 10 25 10 11.46 4.46 8.89 0.285 20 20 10 10 25 20 11.46 4.46 8.66 0.283 10 20 10 10 25 20 11.65 4.46 8.66 0.283 10 10 10 25 20 11.65 4.56 8.66 0.283 20 10 10 25 25 25 25 25 25 30 30 30 30 30 30 30 30 30 30 30 30	₹	1679	52	20	10	9	91	25			•	11.45	4.45	8.92	0.286	6.21
25 20 10 25 10 11.20 4.37 8.52 0.281 20 20 10 25 15 11.46 4.46 8.88 0.283 20 20 15 10 25 10 11.55 4.56 8.87 0.283 20 20 15 25 10 25 20 11.48 4.49 8.66 0.233 15 20 10 25 20 25 20 11.48 4.49 8.66 0.233 10 20 10 10 25 20 11.65 4.56 8.50 0.234 10 20 10 10 25 30 4.65 4.65 9.06 0.234 10 20 30 30 30 4.65 4.65 9.06 0.234 10 20 30 30 4.65 4.65 4.65 9.06 0.234 10<	¥	1689	30	15	10	01	ឧ	52				11.31	4.40	8.81	0.286	7.21
20 20 10 25 15 11.46 4.46 8.88 0.285 20 10 15 25 10 11.48 4.49 8.68 0.283 15 20 10 25 20 11.48 4.49 8.66 0.23 15 20 10 25 20 11.48 4.49 8.66 0.23 10 10 10 25 20 11.62 4.56 8.50 0.28 5 20 10 10 25 25 20 11.60 4.65 9.06 0.28 6 20 10 10 10 25 25 11.50 4.65 9.06 0.28 7 20 20 30 30 4.63 4.43 4.73 7.71 0.25 8 20 30 40 4.23 4.55 8.75 0.27 8 30 40 4.23	¥	1701	25	20	. 8	10		25	8			11.20	4.37	8.52	0.281	6.75
20 20 15 10 25 10 11.55 4.50 8.87 0.283 20 20 10 15 25 20 11.48 4.49 8.66 0.279 10 20 10 10 25 20 11.65 4.56 8.99 0.284 10 20 10 10 25	₹	1703	20	20	91	01		25	. 31			11.46	4.46	8.88	0.285	5.95
20 20 10 15 25 10 11.48 4.49 8.66 0.279 15 20 10 10 25 20 11.65 4.54 8.65 0.284 10 20 10 10 25 25 25 11.62 4.56 8.65 0.276 0 20 10 10 25 30 30 4.65 4.65 9.06 0.284 1 20 10 10 30 30 30 11.30 4.65 3.71 0.250 2 20 10 30 30 40 11.31 4.78 8.75 0.250 2 10 30 40	₹.	7171	20	20	15	01		25	10			11.55	4.50	8.87	0.283	6.48
15 20 10 25 20 11.65 4.56 8.59 0.284 10 20 10 25 25 25 25 25 25 25 25 25 25 26 8.55 8.55 9.06 0.276 5 20 10 10 25 30 30 4.65 4.65 9.06 0.281 20 20 10 20 35 36 4.63 7.71 0.250 20 10 30 40 30 4.65 4.78 8.75 0.27 20 10 30 40 4.78 4.78 8.12 0.26 20 10 20 20 20 4.48 8.12 0.26 20 10 20 20 20 4.48 8.14 0.26 20 10 20 20 20 4.48 8.14 0.26 20 10 </th <th>±</th> <th>1719</th> <th>20</th> <th>02</th> <th>91</th> <th>15</th> <th></th> <th>25</th> <th>10</th> <th></th> <th></th> <th>11.48</th> <th>4.49</th> <th>8.66</th> <th>0.279</th> <th>6.07</th>	±	1719	20	02	91	15		25	10			11.48	4.49	8.66	0.279	6.07
10 20 10 25 25 25 30 11.62 4.56 8.65 0.276 5 20 10 10 25 30 11.90 4.65 9.06 0.281 0 20 10 10 30 30 30 4.63 7.71 0.250 20 10 20 35 35 36 4.63 4.63 7.54 0.250 20 10 30 40 11.31 4.42 8.52 0.279 20 10 30 40 11.31 4.42 8.52 0.275 20 10 20 45 4.55 4.57 8.07 0.262 20 10 20 20 20 11.30 4.45 8.12 0.268 20 10 20 20 11.30 4.45 8.14 0.268 20 10 20 20 20 20 20	•	1729	15	20	10	10		52	20			11.65	4.54	8.39	0.284	. 5.62
5 20 10 10 25 30 11.90 4.65 9.06 0.281 0 20 10 10 30 30 4.63 7.71 0.250 20 20 10 35 35 36 4.63 7.74 0.250 20 10 30 40 11.31 4.42 8.52 0.256 20 10 30 40 11.52 4.57 8.07 0.262 20 10 20 45 4.5 4.78 8.82 0.271 20 10 20 20 20 20 20 20 20 20 10 40 11.30 4.45 8.14 0.268 20 10 20 20 20 4.45 8.14 0.268 20 10 20 20 20 20 20 20 20 20 10 20 20 <th>7</th> <th>1733</th> <th>91</th> <th>20</th> <th>10</th> <th>01</th> <th>•</th> <th>25</th> <th>52</th> <th></th> <th></th> <th>11.62</th> <th>4.56</th> <th>8.65</th> <th>0.276</th> <th>4.85</th>	7	1733	91	20	10	01	•	25	52			11.62	4.56	8.65	0.276	4.85
0 20 10 10 30 30 11.56 4.63 7.71 0.250 20 20 5 35 36 35 36 11.31 4.42 8.52 0.279 20 10 30 40 11.52 4.39 7.54 0.256 20 10 25 45 20 11.36 4.78 8.82 0.271 20 10 20 20 20 11.36 4.45 8.14 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 26.25 35 8.75 10.52 4.25 6.88 0.245 20 10 5.0 10.78 4.26 6.88 0.245	4	1734	ιΩ	20	91	01		52	30		••	11.90	4.65	9.06	0.281	4.35
20 20 5 35 30 4.42 8.52 0.279 20 10 35 35 40 11.04 4.39 7.54 0.256 20 10 40 40 11.52 4.57 8.07 0.262 20 10 30 20 20 11.36 4.48 8.12 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 26.25 35 5.0 10.78 7.63 7.63	<u>.</u>	1772	0	. 20	10	10		30	30			11.56	4,63	1.71	0.250	3.21
20 10 35 35 35 11.04 4.39 7.54 0.256 20 10 25 45 12.14 4.78 8.82 0.271 20 10 20 20 20 11.36 4.48 8.12 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 26.25 35 40 11.30 4.45 8.14 0.268 20 10 30 30 35 5.0 10.78 4.26 7.63 0.263	4	1780	•	20	20	S	-	35	30	•		. 11.31	4.45	8.52	0.279	2.94
20 10 25 45 11.52 4.57 8.07 0.262 20 10 25 45 20 11.36 4.48 8.12 0.268 20 10 20 20 20 11.36 4.48 8.12 0.268 20 10 30 40 11.30 4.45 8.14 0.268 20 10 26.25 35 8.75 10.52 4.22 6.88 0.245 20 10 30 35 5.0 10.78 4.26 7.63 0.263	≟	1787		20	91			35	35			11.04	4.39	7.54	0.256	2.88
20 10 25 45 12.14 4.78 8.82 0.271 20 10 20 20 20 11.36 4.48 8.12 0.268 20 10 40 11.30 4.45 8.14 0.268 20 10 26.25 35 8.75 10.52 4.22 6.88 0.245 20 10 30 35 5.0 10.78 4.26 7.63 0.263	₹	1788	•	50	01			30	04			11.52	4.57	8.07	0.262	2.94
20 10 30 20 · 20 11.36 4.48 8.12 0.268 20 10 30 40 11.30 4.45 8.14 0.268 20 10 26.25 35 8.75 10.52 4.22 6.88 0.245 20 10 30 35 5.0 10.78 4.26 7.63 0.263	7	1789		20	10		•	52	45		-	12.14	4.78	8.82	0.271	3,13
20 10 30 40 11.30 4.45 8.14 0.268 20 10 26.25 35 8.75 10.52 4.22 6.88 0.245 20 10 30 35 5.0 10.78 4.26 7.63 0.263	±	1824	•	20	10			30	. 02	02		11.36	4.48	8.12	0.268	3.02
20 10 26.25 35 8.75 10.52 4.22 6.88 0.245 20 10 30 35 5.0 10.78 4.26 7.63 0.263	₹	1825		70	.ន			30		40		11.30	4.45	8.14	0.268	3.22
- 20 10 30 35 5.0 10.78 4.26 7.63 0.263	₹	1847		20	2			26.25	32		8.75	10.52	4.22	6.88	0.245	2.84
	₹.	1848 -	•	20	8			S	35		5.0	10.78	4.26	7.63	0.263	2.69

PATEIIT DISCLOSURE

Low Compressibility, Low Expansivity Glasses

Douglas Blackburn, Albert Feldman Glass and Optical Materials Group National Bureau of Standards

and

Nicolas Lagakos Physical Acoustics Branch Naval Research Laboratory

A series of beryllium-free glasses have been formulated that exhibit a high Young's modulus (E), a high bulk modulus (K), and a wide range of expansivities. Several of the glasses exhibit unusually small linear thermal expansion coefficients (α) at room temperature. The glasses were formulated with the view of not including BeO as a constituent because of its potential toxicity.

Formulations:

The compositions fall in the following weight percent ranges:

CaO ₂	0 - 30%
A1 ₂ 03	15 - 25%
MgÖ Ö	5 - 15%
TiO ₂	0 - 15%
ZrO ₂	0 - 10%
SiO2	20 - 30%
B ₂ 0 ₃	0 - 10%
Ta ₂ 0 ₅	0 - 45%
Nb205	0 - 40%

Particular compositions show desirable combinations of properties. The highest Young's modulus was exhibited by the glass with the following composition:

A1 ₂ 0 ₃	20%	$E = 12.1 \times 10^{11} \text{ dyn/cm}^2$
Mg0	10%	$K = 8.8 \times 10^{11} \text{ dym/cm}^2$
SiO ₂	25%	$\alpha = 3.1 \times 10^{-6} / ^{\circ} \text{C}$ at 20 °C
Ta ₂ 0 ₅	45%	•

The highest bulk modulus was exhibited by the glass with the following composition:

Ca0	5%	
A1203	20%	$E = 11.9 \times 10^{11} \text{ dym/cm}^2$
Mg0	10%	$K = 9.1 \times 10^{11} \text{dym/cm}^2$
Ti ₂ 0 ₃	10%	$\alpha = 4.4 \times 10^{-6} / ^{\circ} \text{C at } 20 ^{\circ} \text{C}$
SiO ₂	25%	•
Ta ₂ 0 ₅	30%	

The smallest linear thermal expansion coefficient was exhibited by the glass with the following composition:

A1 ₂ 0 ₃	20%	· _
MgÖ	10%	$E = 10.8 \times 10^{11} \text{ dym/cm}^2$
Si0 ₂	30%	$K = 7.6 \times 10^{11} \text{ dym/cm}^2$
Ta ₂ 0 ₅	35%	$\alpha = 2.7 \times 10^{-6}$ /°C at 20 °C
B ₂ 0 ₃	· 5%	•

The following glass composition was optimized to possess a large bulk modulus and a small linear thermal expansion coefficient:

A1203	20%			
Mg0	10%			Oldon/cm ²
T10 ₂	5%			0 ¹¹ d yn/ cm ²
510,	35%	a =	2.9 x 1	0 ⁻⁶ /°C at 20 °C
Ta ₂ 0 ₅	30%			

Uses:

- (1) Glasses for graded seals. Thermal expansion coefficients at 20 °C in the range 2.7×10^{-6} to 7.2×10^{-6} are obtainable.
- (2) Temperature stable optical glass. Because the melts of the glasses described herein are of low viscosity, it is possible to produce homogeneous glasses possessing low expansivities. The expansivity of the glass with the smallest expansion coefficient approximates the expansivity of Pyrex. However, because of its high melt viscosity, Pyrex is not usable as a high quality optical glass.
- (3) Pressure insensitive fibers. Cladding glasses with high bulk modulus are required to produce fibers that are insensitive to pressure fluctuations. Typically, fiber cores are made from high silica glasses, which have very small expansivities; thus, in order to produce mechanically stable fibers, with these core glasses, it is necessary to use cladding glass with small expansivities. The glasses described herein can be produced both with high bulk modulus and low expansivity thus increasing the probability for successful drawing of pressure insensitive fibers.

Importance of Pressure Insensitive Fibers

A major research effort is underway, especially at the Department of Defense, for development of fiber-optic sensors as an alternate technology to current sensor technology. Such sensors would be used for sensitive detection of pressure, temperature, electric fields and magnetic fields. These sensors require special fiber-optic cables for transmission and reception of sensor signals over distances of several kilometers. Over such large distances, fluctuations in the ambient pressure will lead to superimposition of noise on the sensor signal. Thus fiber-optic cables insensitive to these pressure fluctuation are required for maximizing the signal to noise ratio in the received signals. Immediate potential applications for these fibers would be underwater acoustic detection, acoustic detection related to underground nuclear explosions, and earthquake detection.

PONM CE-240	U.S. DEPAR	THENT OF COMMERCE	FOR PATENT	ADVISER'S	USE
THE S. BY CAO TOA ? STA			Case No.		
INVENTION DISCLOSURE AND	RIGHTS QUESTION	NAIRE			
•					
INSTRUCTIONS: Complete and send to Patent	Adviser, Office of the	Legal Adviser, Nation	al Bureau of Standards.	,	
Washington, D.C. 20234.	•				
Title of Invention (Attach full description)	***	*	· ·		
Low Compressibility, Low Expan	sivity Glasses				
Inventor		Title and Grade	· · · · · · · · · · · · · · · · · · ·		
Douglas Blackburn		Chemist, GS-1			
Division Name Materials Chemistry Division		Building Matls/223	Room No. B316	X.2817	
Inventor		Title and Grade	1 2310	X.2017	
Albert Feldman		Physicist, GS	-15	· · ·	
Division Name		Building Room No.	Room No.	Telephone	
Materials Chemistry Division		Mat1s/223 Title and Grade	A249	x.2817	
Nicolas Lagakos		Physicist, GS	-13		
Division Name		Building	Room No.	Telephone	
Naval Research Laboratory	·	71	Code 5134	767-31	79
	STATEMENT O	F INVENTOR(S)	rmal report	Yes	No
1. Has the invention been published? (Attach	copy of paper, preprint,				Y
2. Has the invention been used only experimen	h=112				
2. Has the invention peen used only experimen	Cally!			X	
3. Do you know of relevant prior art? (Attach o	· NBS Report	No. 5188 (1957)	X	
4. Was the invention sponsored by another ager		nd Order No.) Naval	Research Lab.	X	
5. Does the invention bear a direct relation to attach copy of position description)		110017	<u> </u>	×	
stach copy of position description)					
6. Was the invention made					
A. During working hours		<u>.</u>			
				X	<u> </u>
B. With a contribution by the government of					
e. Facilities				x	
1. Forderson				X	
b. Equipment c. Materials				l x	
d. Funds				X	
e. Information available only by reason	of your official duties			x	
f. Time or services of other government		duty		X	
7. Estimate the market for the invention.					
Selling price \$	_ x Number of sales_		_= Market \$ 10M-100		
A	Signature Douglas Black	burn D.	De Olin	Date 9-	20-82
	Douglas Black		practive	Date	
8. CERTIFICATION OF INVENTOR(S) Albert Feldman albut Jeldman 9-17-8					1-82
H	Signature	os Nikolae Lag		0ate 7-20	-82
			us purs.	ـــــــــــــــــــــــــــــــــــــ	
	SUPERVISORY CO	JACURKENCE		Yes	No
9. Do you agree with the replies to questions I	- 7?				
10. Are you aware of any question as to inventor	rship?			1	1
Signature of Supervisor	Date	Signature of Division		Date	>
•		120 Coyle		9/21	182

DATE ILME